

July 13, 2010

In Reply Refer To: HSSD/B-207

Carl Eugene Buth, Ph.D., P.E. Assistant Agency Director Texas Transportation Institute The Texas A&M University System 3135 TAMU College Station, TX 77843-3135

Dear Dr. Buth:

This letter is in response to your most recent request for the Federal Highway Administration (FHWA) acceptance of the following proposed retrofit design of an existing Ohio Department of Transportation (ODOT) Standard Bridge Railing for use on the National Highway System (NHS).

Name of system:	Modified Ohio DOT (ODOT) Deep Beam Bridge Railing (Guardrail Barrier)	
Type of system:	Post and Tube with W-Beam Permanent Barrier	
Test Level:	NCHRP Report 350 Test Level 3 (TL-3)	
Testing conducted by:	<i>x</i> : Acceptance based on Equivalence via Strength Analysis and nonlinear finite	
	element simulation using LS-DYNA as conducted by Texas Transportation	
	Institute	
System Designator:	SBB08c	
Date of request:	May 15, 2010	

Requirements

Roadside safety systems should meet the guidelines contained in the National Cooperative Highway Research Program (NCHRP) Report 350, "Recommended Procedures for the Safety Performance Evaluation of Highway Features". The FHWA memorandum "<u>ACTION</u>: Identifying Acceptable Highway Safety Features" of July 25, 1997, provides further guidance on crash testing requirements of longitudinal barriers. In addition, roadside safety system structural analysis of bridge railings for crashworthiness is also permissible as per the May 16, 2000 FHWA memo entitled Bridge Rail Analysis.

Description

The ODOT Deep Beam Bridge Guardrail Barrier is a post and tube with w-beam panel permanent barrier system measuring 30 inches high. This bridge barrier is listed as the Ohio Box Beam Rail in the FHWA memorandum for Bridge Rails dated August 28, 1986, and was successfully crash tested



under NCHRP Report 230 as a Performance Level 1 (PL1) bridge barrier. The PL1 railing has an equivalency of Test Level 2 (TL-2) per FHWA memorandum "Crash Testing of Bridge Railings" dated May 30, 1997. A combination of analytical study and computer simulation was utilized to evaluate the performance of the ODOT Deep Beam Bridge Guardrail Barrier. The final product is a modified design of the ODOT Deep Beam Bridge Guardrail Barrier system (retrofit) to bring this modified system into compliance with the NCHRP Report 350 performance criteria for TL-3.

The existing bridge rail design was reviewed to investigate the performance aspects of all similar railing systems successfully crash tested as per NCHRP Report 350. The investigation revealed railing systems that share some of the characteristics of the ODOT Deep Beam bridge rail including the Texas Department of Transportation (TxDOT) Type T101, the Illinois side-mount rail and the Oregon side-mount bridge rail. The Illinois side-mount bridge rail design was chosen for the analysis comparison. The Illinois Side-Mount barrier consists of W6x25 (W 150x37.1) posts spaced at 6 ft-3 in. (1.905 m) with two tubular rails, TS 8x4x5/16 in. (203x102x8 mm) for the top rail and TS 6x4x1/4 in. (152x102x6 mm) for the lower rail. The height of the top rail above the asphalt surface is 32 inches (813 mm). The railing was mounted to the side of a concrete deck using four (4) AASHTO MI64 anchors bolts. The Illinois side mounted bridge rail was successfully tested to AASHTO PL-2 including the single unit truck.

After review and analysis of the existing ODOT Deep Beam Bridge Railing (Guardrail Barrier) system, the suggested retrofit is the addition of two (2) additional tubular members to help improve the performance of the ODOT Deep Beam bridge rail. The following two rail members have been added to in such a way as to utilize the current bridge rail hardware and minimize retrofitting the existing bridge rail post.

- A. One tubular member added at 8 in. (230 mm) above the pavement surface to improve the crash performance for the small car (820C) in NCHRP Report 350 TL-3 conditions.
- B. One tubular member added to top of existing tubular block out to increase the overall height to 31 in. (787.4 mm) above the pavement surface. Increasing the height of the bridge rail is considered to be an improvement in crash performance by the design team particularly for impact conditions that involve the pick-up truck (2000P).

Strength analyses were then conducted to determine the strength of the retrofit rail design with respect to AASHTO Bridge Design Specification. Developed details for analysis of the 16 in. (406.4 mm) concrete deck were approved by ODOT and incorporated into the analyses for the retrofit bridge rail design. The 2004 AASHTO LRFD Bridge Design Specifications, Table 13.7.2-1 and Table A13.2-1 were used to calculate the strength of the modified ODOT Deep Beam Bridge Guardrail Barrier system, and is included as an enclosure with this correspondence.

A detailed LS-DYNA finite element model was built for the ODOT deep beam post assembly. The assembly includes the W6x25 (Wl50x37.1) post, the stiffening plates, the 1-1/4 in. (31.75 mm) diameter A325 anchor bolt, the 16 in. (406.4 mm) deck and the detailed reinforcement per the system drawings enclosed with this correspondence.

Based on the LS-DYNA numerical analysis and engineering analysis, it is expected the post-deck assembly would have the capacity to withstand the 54kips (240 kN) load imparted by the 2000P test vehicle (per NCHRP Report 350 TL-3) without significant damage.

A full model of a representative installation of the modified ODOT Deep Beam bridge rail per NCHRP Report 350 test requirements for rigid barrier was built. The model consists of a 75 ft (22.86 m) long rail that includes six w-beam rail segments and 13 (thirteen) post assemblies.

The system was able to contain and redirect the vehicle per the finite element simulation. The vehicle had a moderate roll angle (18 degrees) around 0.52 seconds (sec) but it became upright late in the simulation. The simulation calculated the maximum tensile force in the deck anchors to be 88.91 kips (395 kN). This is below the yield rating of these anchors of 99 kips (440.4 kN) as presented in strength analysis. The summary of results of TL-3-11 simulation is also enclosed with this correspondence.

Findings

We concur that based upon equivalence and computation the modified ODOT Deep Beam Bridge Guardrail Barrier meets all barrier structural adequacy and vehicle trajectory criteria as outlined in NCHRP Report 350 and is acceptable for use on the NHS as a TL-3 barrier when allowed by the highway agency. Please note the following standard provisions that apply to FHWA letters of acceptance:

- This acceptance is limited to the crash worthiness characteristics of the system and does not cover their structural features, nor conformity with the Manual on Uniform Traffic Control Devices.
- Any changes that may adversely influence the crashworthiness of the system will require a new acceptance letter.
- Should the FHWA discover that the qualification testing was flawed, that in-service performance reveals unacceptable safety problems, or that the system being marketed is significantly different from the version that was crash tested, we reserve the right to modify or revoke our acceptance.
- You will be expected to supply potential users with sufficient information on design and installation requirements to ensure proper performance.
- You will be expected to certify to potential users that the hardware furnished has essentially the same chemistry, mechanical properties, and geometry as that submitted for acceptance, and that it will meet the crashworthiness requirements of the FHWA and the NCHRP Report 350.
- To prevent misunderstanding by others, this letter of acceptance is designated as number B-207 and shall not be reproduced except in full. This letter and attached computational documentation upon which it is based are public information. All such letters and documentation may be reviewed at our office upon request.
- This acceptance letter shall not be construed as authorization or consent by the FHWA to use, manufacture, or sell any patented system for which the applicant is not the patent holder. The acceptance letter is limited to the crashworthiness characteristics of the candidate system, and the

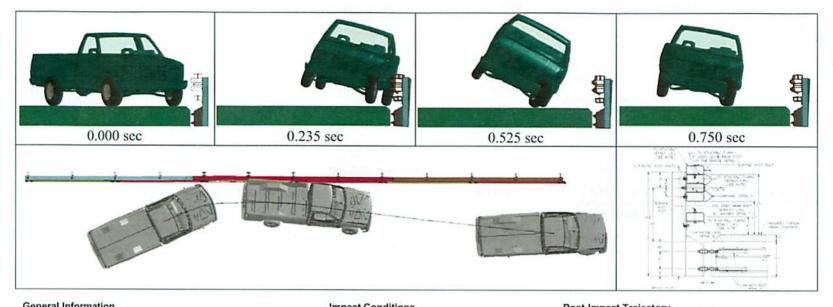
FHWA is neither prepared nor required to become involved in issues concerning patent law. Patent issues, if any, are to be resolved by the applicant.

Sincerely yours,

David A. Nicol, P.E. Director, Office of Safety Design



Office of Safety



36

General Information		Impact 0
Test Agency	Texas Transportation Institute	Speed
Test No.	TL-3-11	Angle.
Date		Locatio
Test Article	N/A	Exit Cor
Туре		Speed
	31 in. Modified Ohio Deep Beam	Angle.
Name	Bridge Rail	Occupa
Installation Length		Impact
Material or Key Elements	75 ft	Long
	bridge rail supported by W6x25	Late
Soil Type and Condition	steel post	Ridedo
Test Vehicle		Long
Type/Designation		Late
Make and Model	2000P	THIV
Curb	C2500 detailed vehicle	PHD
Test Inertial	4408 lb	Max. 0.0
Dummy		Long
Gross Static		Late
	4408 lb	Verti

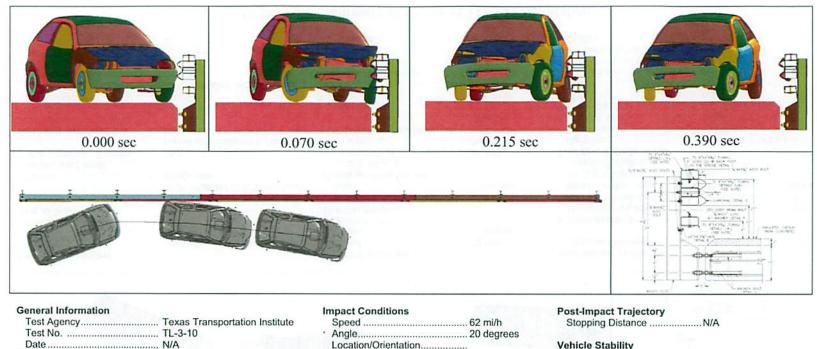
Impact Conditions	
Speed	62 mi/h
Angle	25 degrees
Location/Orientation	
Exit Conditions	
Speed	46.3 mi/h
Angle	5 degrees
Occupant Risk Values	
Impact Velocity	
Longitudinal	
Lateral	28.2 ft/s
Ridedown Accelerations	
Longitudinal	10.9 Gs
Lateral	
THIV	
PHD	
Max. 0.050-s Average	
Longitudinal	11.3 Gs
Lateral	13.7 Gs
Vertical	5.7 Gs

Post-Impact Trajectory Stopping DistanceN/A

Vehicle Stability

Maximum Yaw Angle	29.4 degrees @ 0.294 s
Maximum Pitch Angle	4.1 degrees @ 0.432 s
Maximum Roll Angle	
Vehicle Snagging	No
Vehicle Pocketing	No
Test Article Deflections	
Dynamic	2.56 in. (top of barrier)
Permanent	
Working Width	2.56 in.
Vehicle Damage	
VDS	N/A
CDC	
Max. Exterior Deformation	N/A
Max. Occupant Compartmen	it
Deformation	N/A
OCDI	

Figure 5.28 Summary of results of TL-3-11 Simulation



Exit Conditions

Occupant Risk Values

Max. 0.050-s Average

Ridedown Accelerations

Impact Velocity

		100	1.00	1.20	1000 M
Vel	hic	:le	S	tah	ility

Maximum Yaw Angle 29.	2 degrees @ 0.399 s
Maximum Pitch Angle 3.0	degrees @ 0.226 s
Maximum Roll Angle 4.0	degrees @ 0.314 s
Vehicle SnaggingNo	
Vehicle Pocketing No	
Test Article Deflections	
Dynamic0.75	in 8 in
PermanentN/A	
Working WidthN/A	
Vehicle Damage	
VDSN/A	
CDCN/A	
Max. Exterior Deformation N/A	
Max. Occupant Compartment	
Deformation	
OCDIN/A	

Figure 5.35 Summary of results of 3-10 simulation of the bridge rail with pavement overlay

Longitudinal 5.8 ft/s

Lateral.....-8.8 ft/s

Longitudinal-7.0 Gs

Longitudinal-10.8 Gs

Vertical.....-4.1 Gs

PHD 12.4 Gs

Test Article

Test Vehicle

Name.....

Soil Type and Condition.....

Installation Length 75 ft

Make and Model Geo Metro

Dummy No. Dummy

Curb...... 1807 lb

Test Inertial 1807 lb

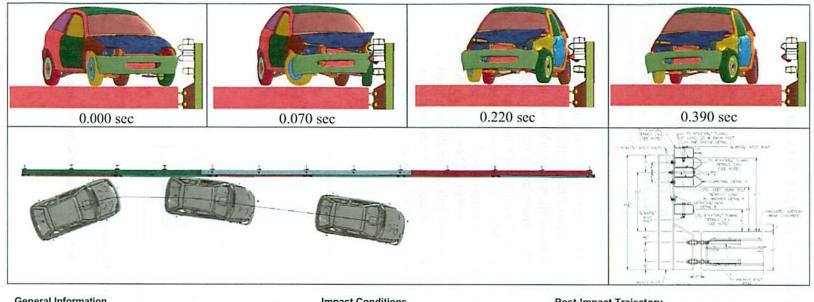
Gross Static 1807 lb

Type...... 31 in. Modified Ohio Deep Beam

Material or Key Elements bridge rail supported by W6x25

Bridge Rail

steel post



46

General Information	
Test Agency	Texas Transportation Institute
Test No.	Simulation
Date	
Test Article	
Туре	34 in. Modified Ohio Deep Beam Bridge Rail
Name	
Installation Length	75 ft
Material or Key Elements	bridge rail supported by W6x25 steel post
Soil Type and Condition	
Test Vehicle	
Type/Designation	
Make and Model	Geo Metro
Curb	
Test Inertial	
Dummy	No. Dummy
Gross Static	

Impact Conditions
Speed 62 mi/h
Angle
Location/Orientation
Exit Conditions
Speed
Angle10 degrees
Occupant Risk Values
Impact Velocity
Longitudinal 5.3 ft/s
Lateral8.6 ft/s
Ridedown Accelerations
Longitudinal6.2 Gs
Lateral 12.6 Gs
THIV
PHD 12.6 Gs
Max. 0.050-s Average
Longitudinal
Lateral 15.6 Gs
Vertical3.9 Gs

Post-Impact Trajectory Stopping DistanceN/A.

Vehicle Stability

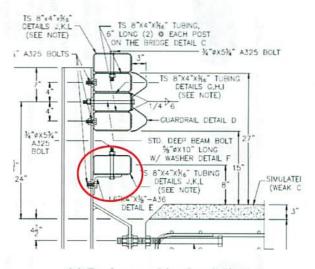
Maximum Yaw Angle	28.4 degrees @ 0.493 s
Maximum Pitch Angle	3.2 degrees @ 0.213 s
Maximum Roll Angle	
Vehicle Snagging	No
Vehicle Pocketing	No
Test Article Deflections	
Dynamic	0.55 in. (top of barrier)
Permanent	
Working Width	N/A
Vehicle Damage	
VDS	N/A
CDC	N/A
Max. Exterior Deformation	N/A
Max. Occupant Compartmen	t
Deformation	N/A
OCDI	N/A

Figure 5.42 Summary of results of 3-10 simulation of the bridge rail without pavement overlay

6. CONCLUSIONS AND RECOMMENDATIONS

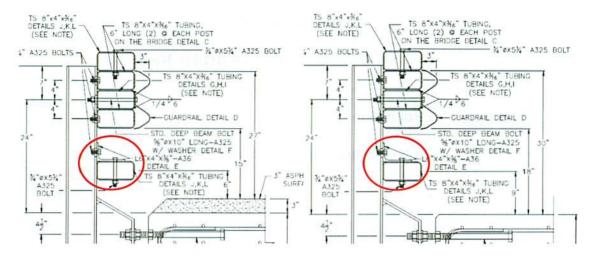
The modified ODOT Deep Beam bridge rail design is shown to be successfully able to pass NCHRP Report 350 test level 3 assessment criteria. This conclusion is based on engineering strength analysis and nonlinear finite element simulation. The added rail on the top of the bridge rail helped reduced potential vehicular dynamics instability that may occur if only the original rail (less height) was used. Also, the additional lower rail (rub rail) provided a protection against tire snagging in the opening below the main rail and the deck. This snagging mode could be detrimental for small vehicle impacts due to the subsequent excessive deformation and increased ridedown acceleration.

The set of drawings of the modified ODOT Deep Beam bridge rail used in the simulation models is shown in APPENDIX C. In this set, lower rail attached to the post using an A36 angle shaped steel plate as shown in Figure 6.1(a). The distance from the middle of this rail to the top of the asphalt overlay is 8 in. (230 mm). However the concern about tire snagging led the researchers to recommend reducing that distance. Therefore, the drawing was modified as shown in Figure 6.1 (b) to reduce the distance from middle of the rub rail to the top of the asphalt overlay to 6 in. (152.4 mm). In the case of an installation without asphalt overlay, the distance from the middle of the rub rail to the top of the deck will be 9 in. (228.6 mm) as shown in Figure 6.1 (c). Consequently, the shelf angle that holds the rub rail in the simulated design would have to be located on the top of the rub rail due to space restriction as shown in Figure 6.1 (b) and (c). The full sets of drawings for the suggested installations are presented in APPENDIX D and APPENDIX E.



(a) Design used in simulation





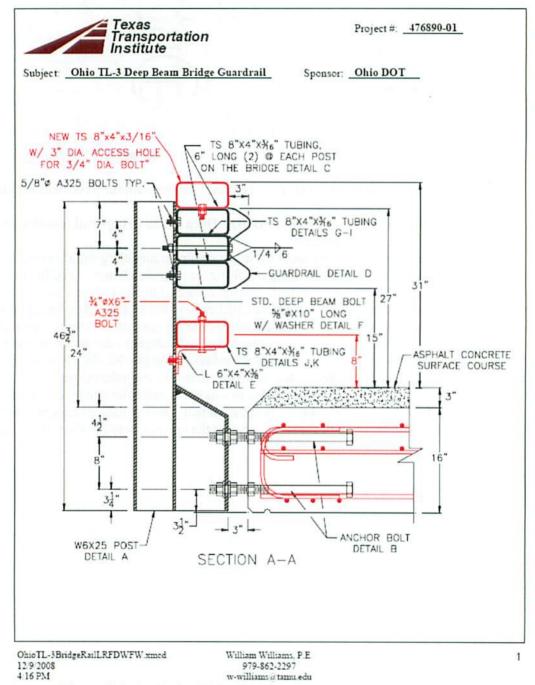
(b) Final design with pavement overlay (c) Final design without pavement overlay

Figure 6.1 Comparison of design of the ODOT Deep Beam bridge rail (continued)

Although details were explicitly modeled in the nonlinear modeling simulation task of this research, some uncertainties are still not quantifiable through simulation. Specifically, damage to the suspension system of the vehicle and the failure of tire and wheels are not represented in current vehicles models. Tire failure (debeading, blown out...etc), wheel failure (rim separation and damage), and suspension failure (A-Arm rupture, joints failure ...etc) can lead to a variation of vehicular dynamical response as well as changes to the occupant severity of a given test. Hence, the research team recommends conducting the two NCHRP Report 350 tests (3-11 and 3-10). For the 3-11 test, the research team recommends using the bridge rail installation that incorporates the pavement overlay to maximize vehicular dynamics. For the 3-10 test, the research team recommends using the bridge rail installation that incorporates the pavement overlay to maximize the potential of snagging of the small car with the opening between the rub rail and the top of the deck.

APPENDIX B

Analysis of ODOT Modified Bridge Rail





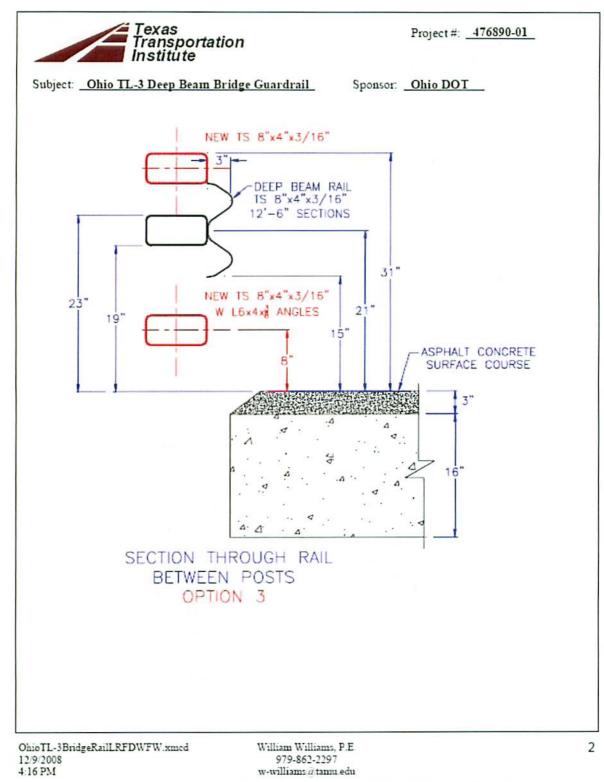
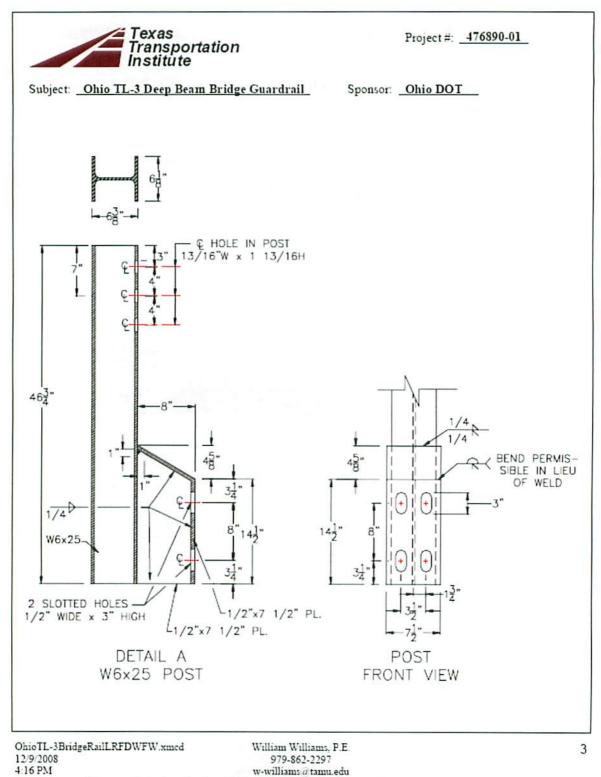
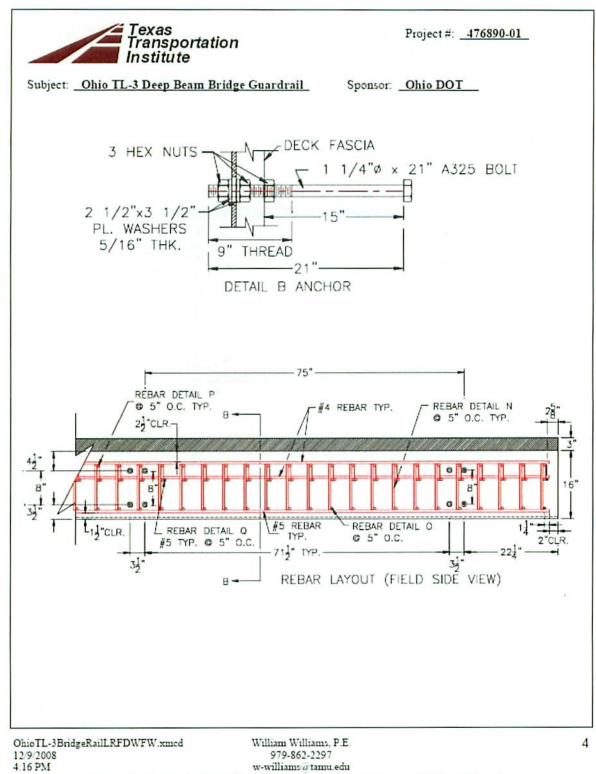


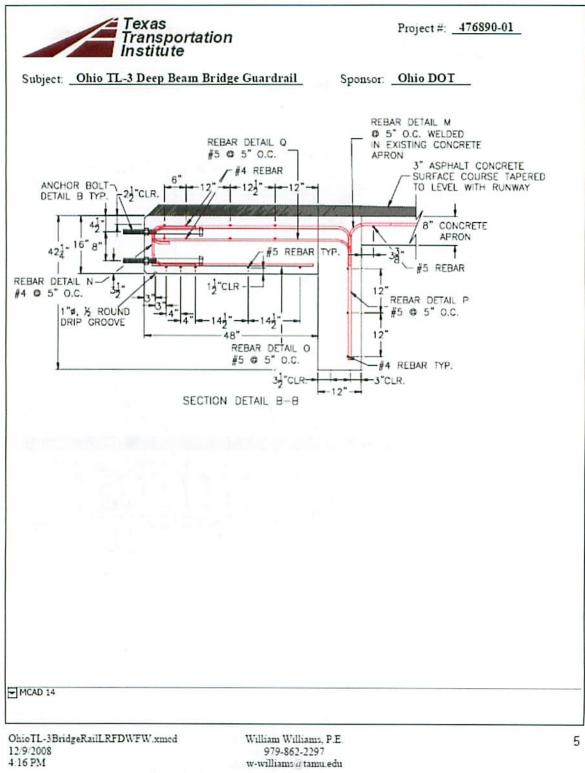
Figure B 2 Analysis of Modified ODOT Deep Beam Bridge Rail 2



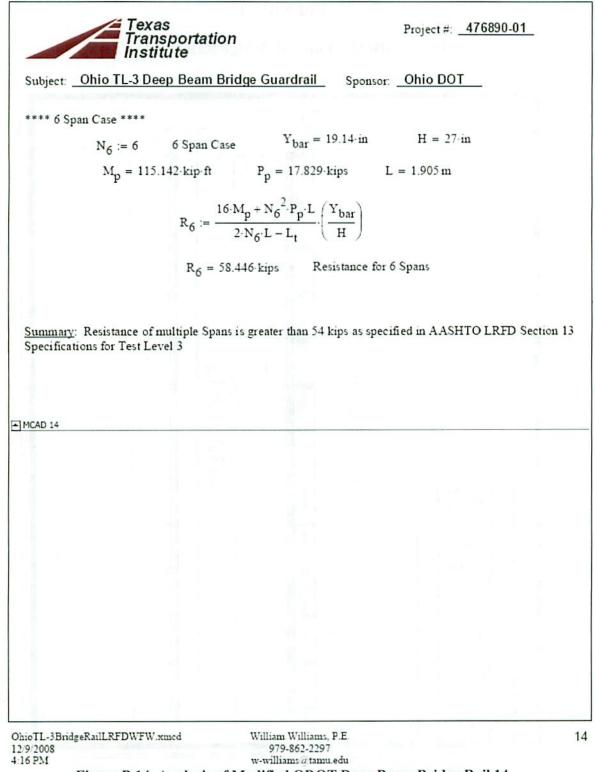






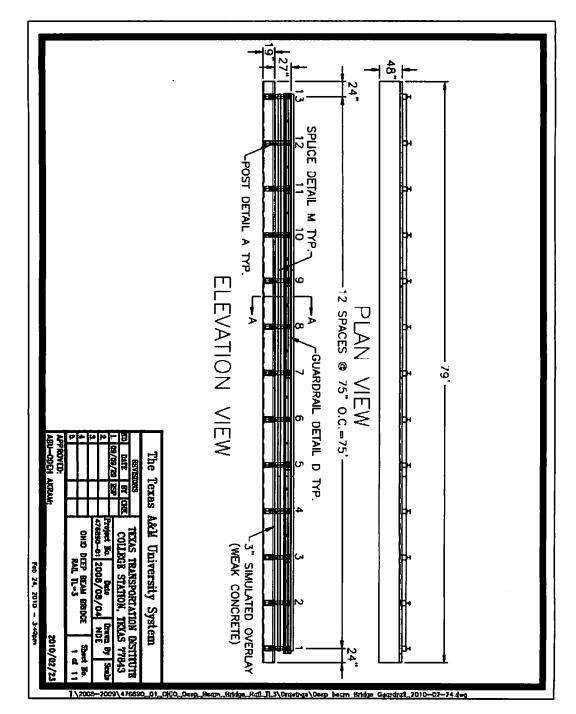




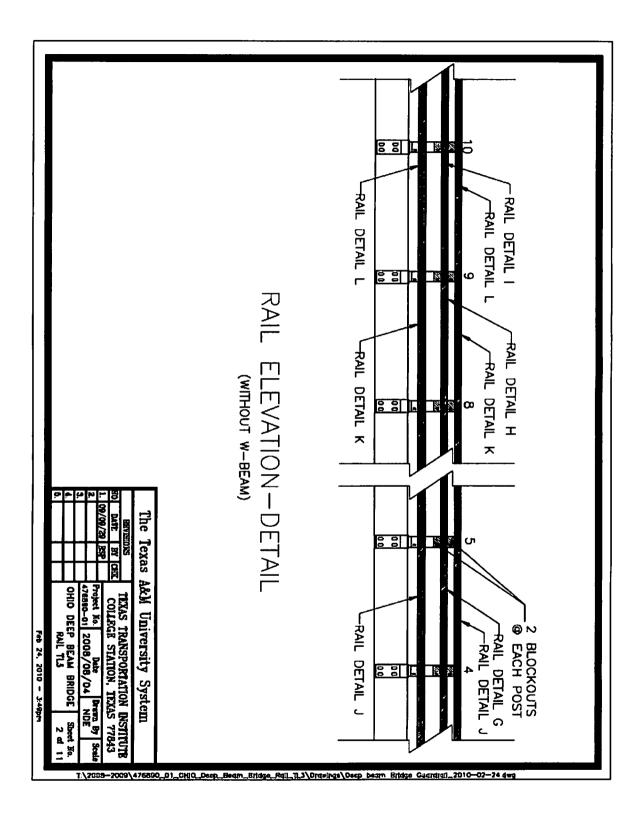


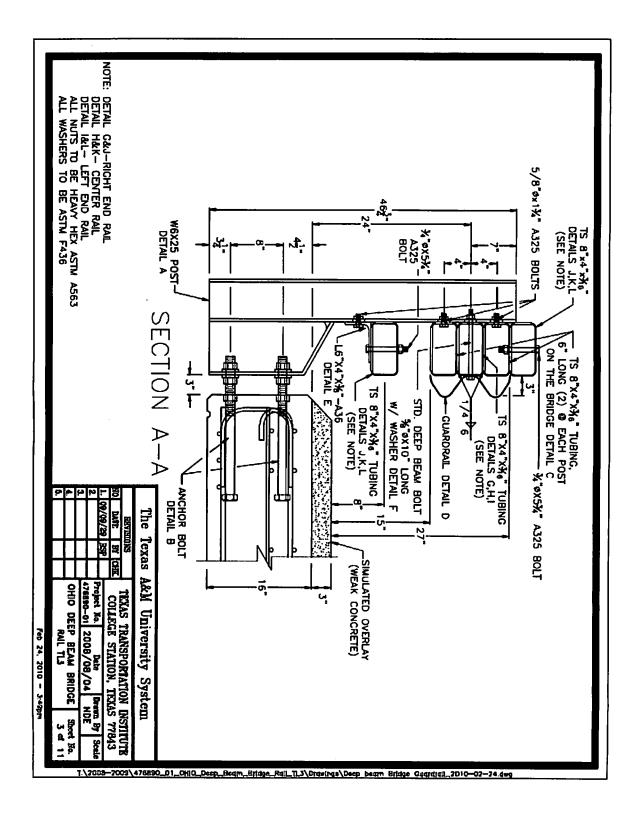


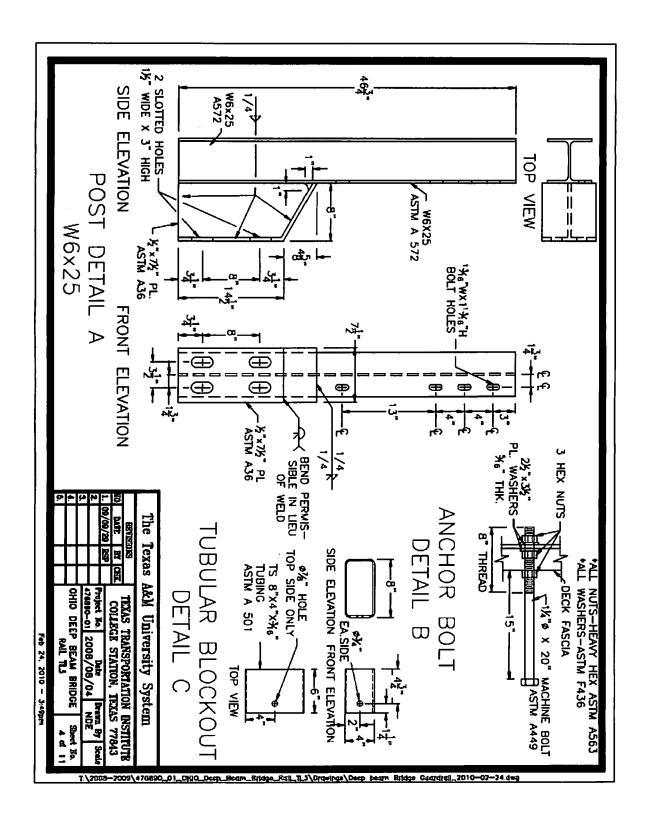


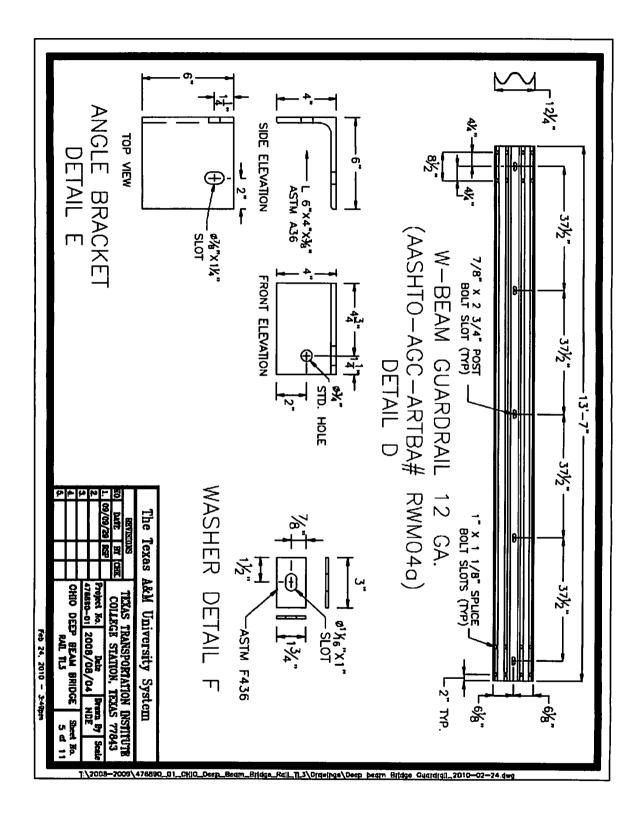


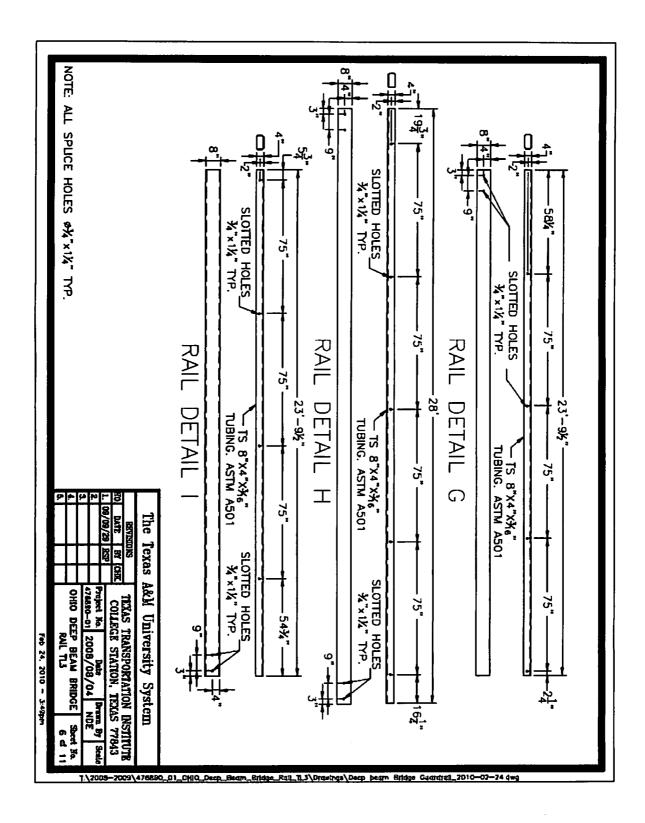


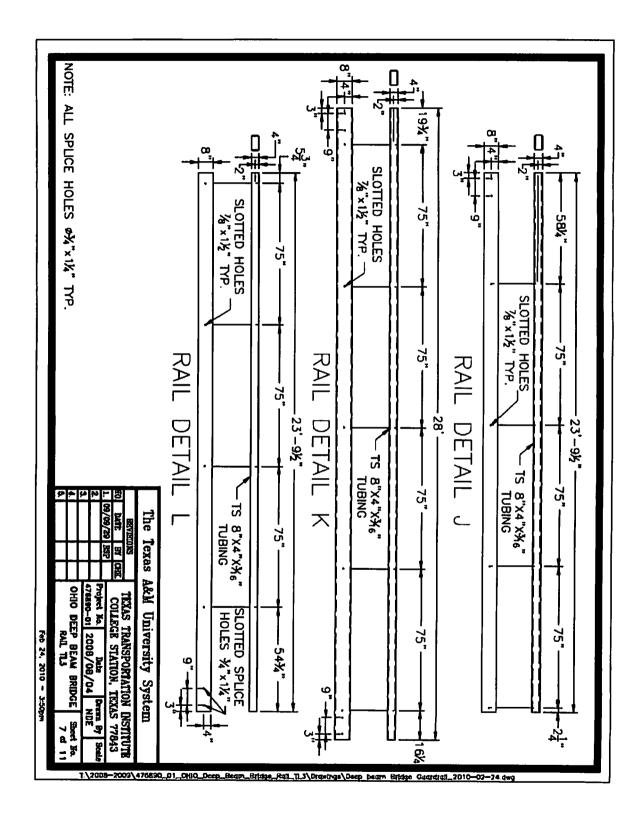


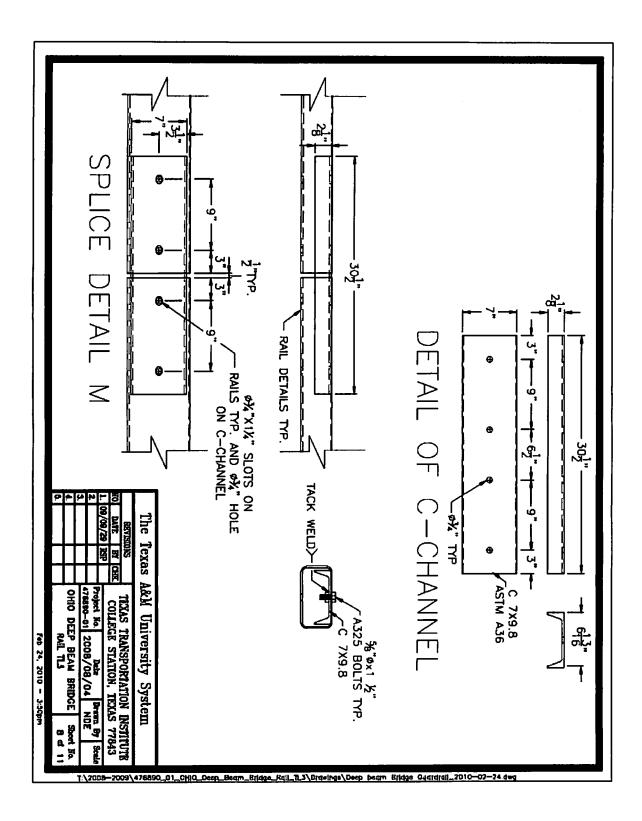


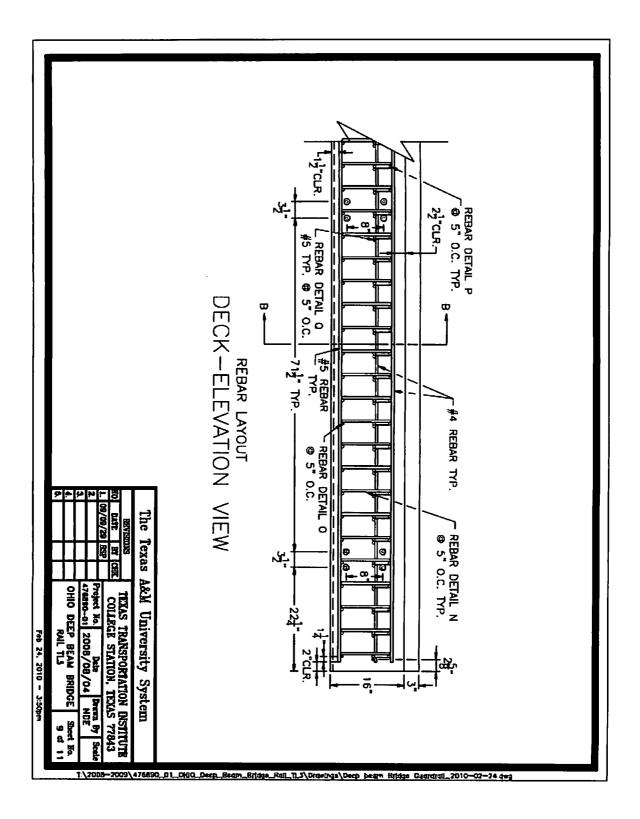


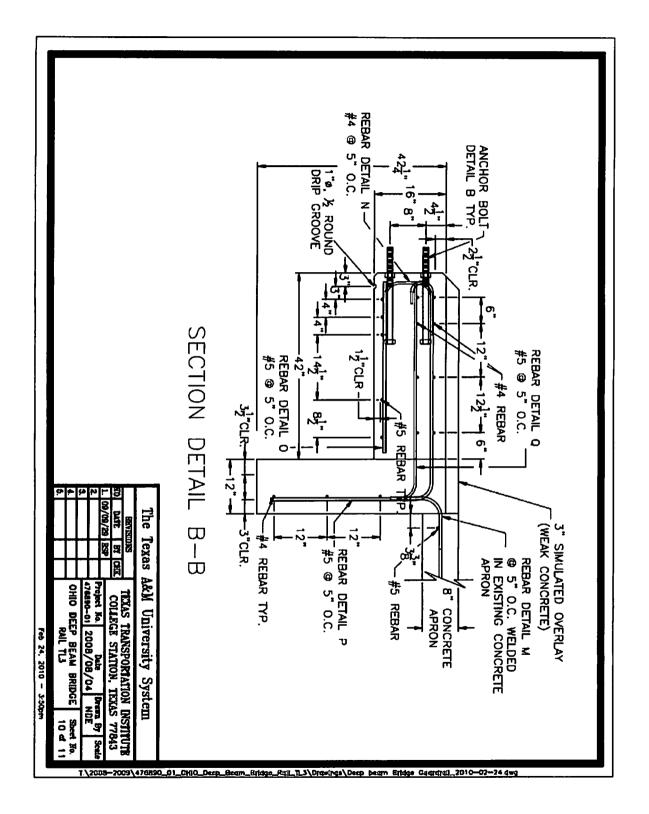


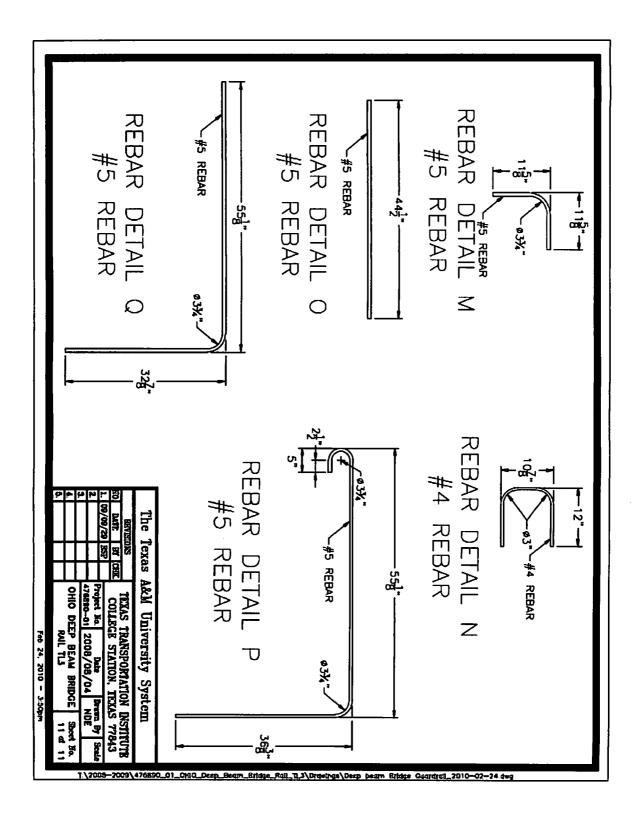




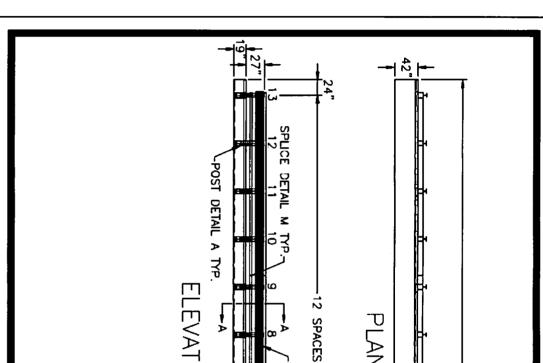




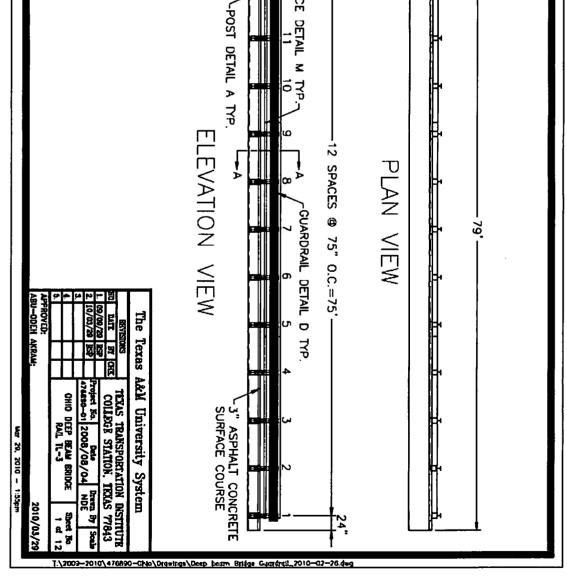


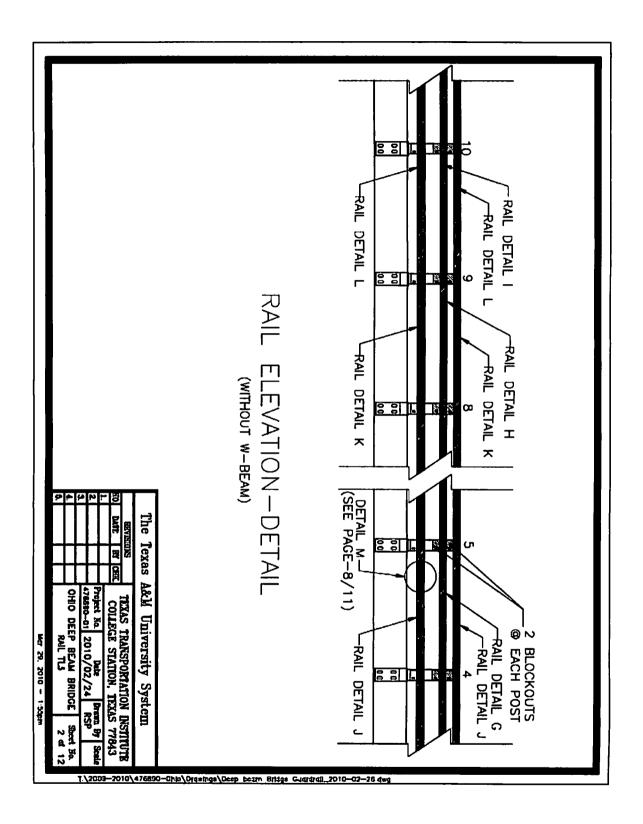


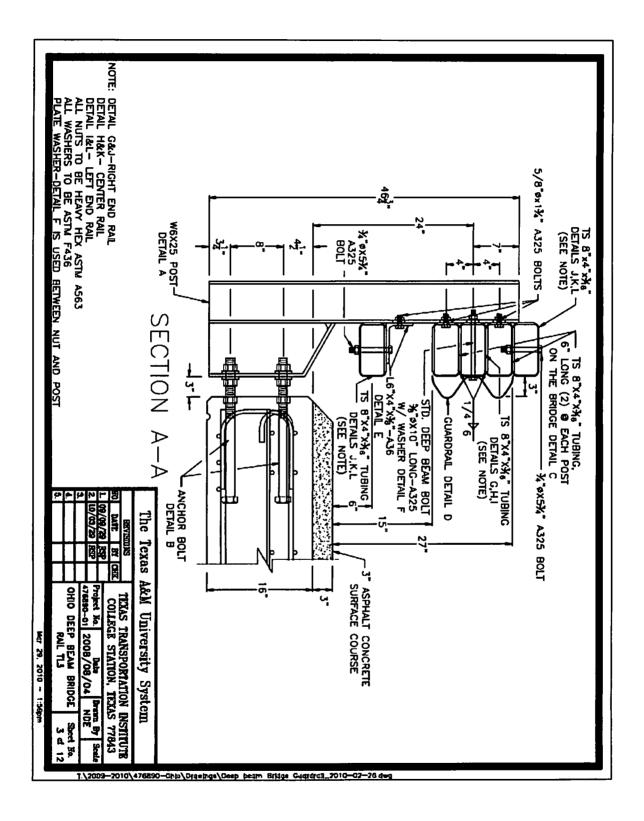
APPENDIX D

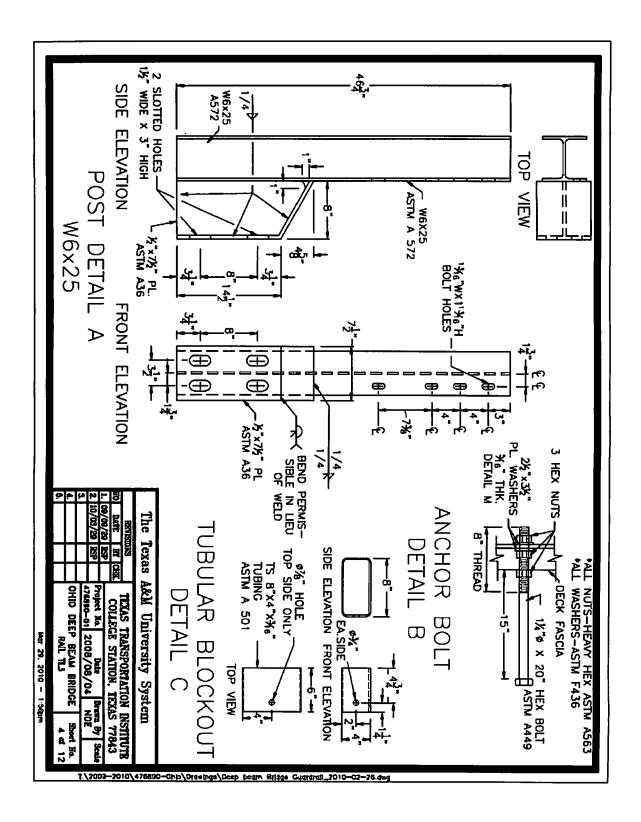


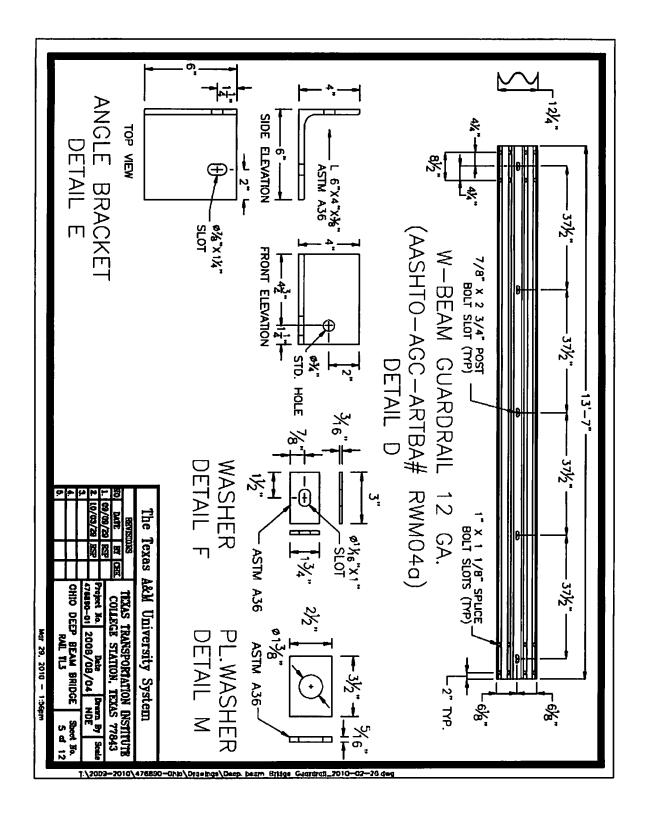
Drawing of ODOT Modified Bridge Rail with Pavement Overlay

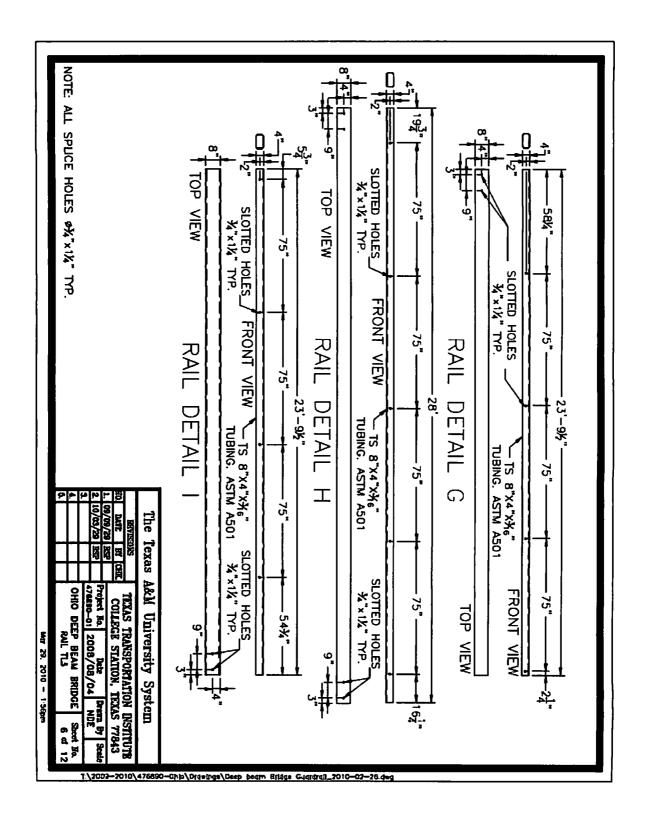


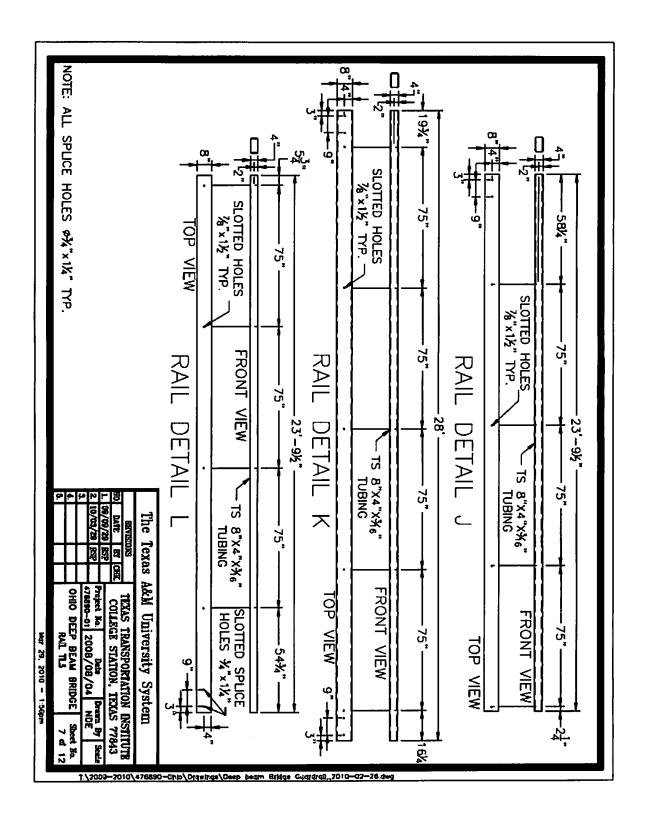


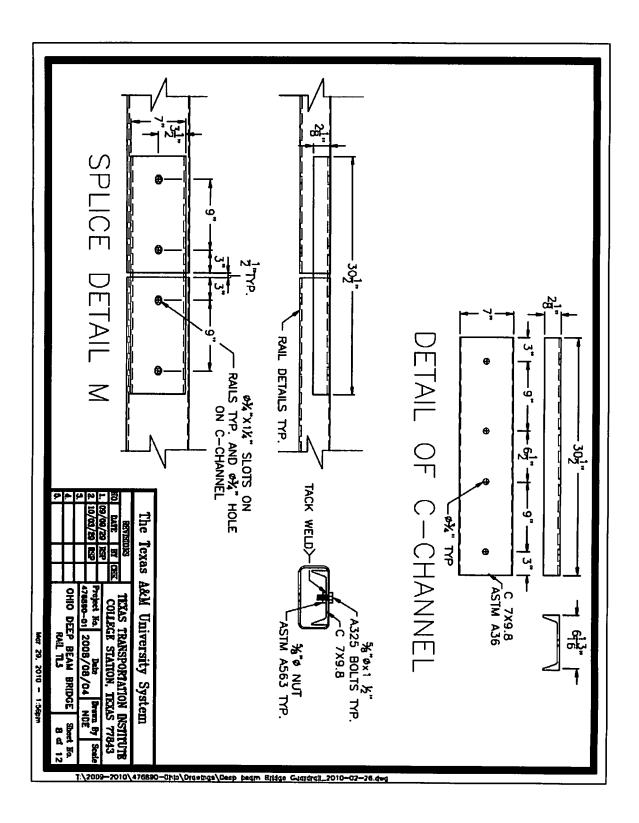


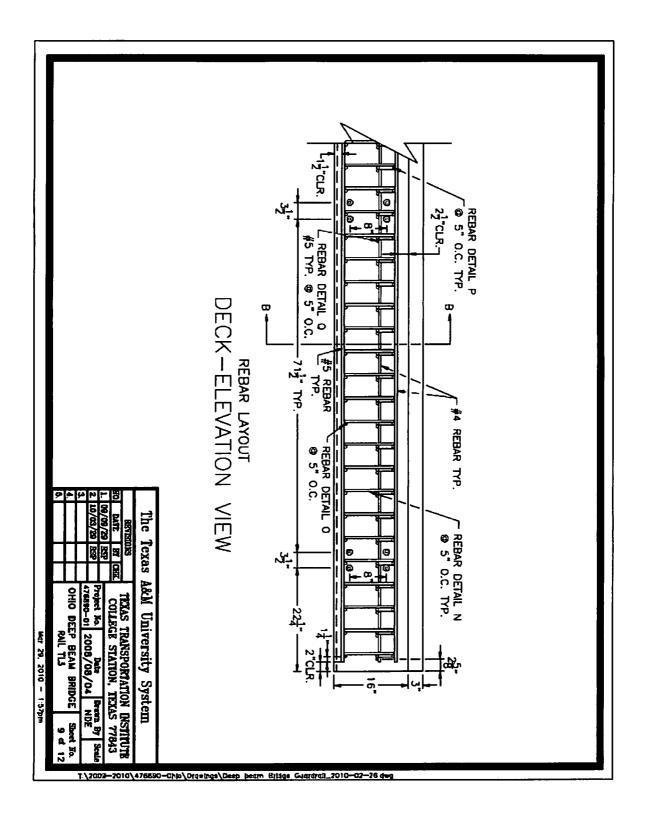


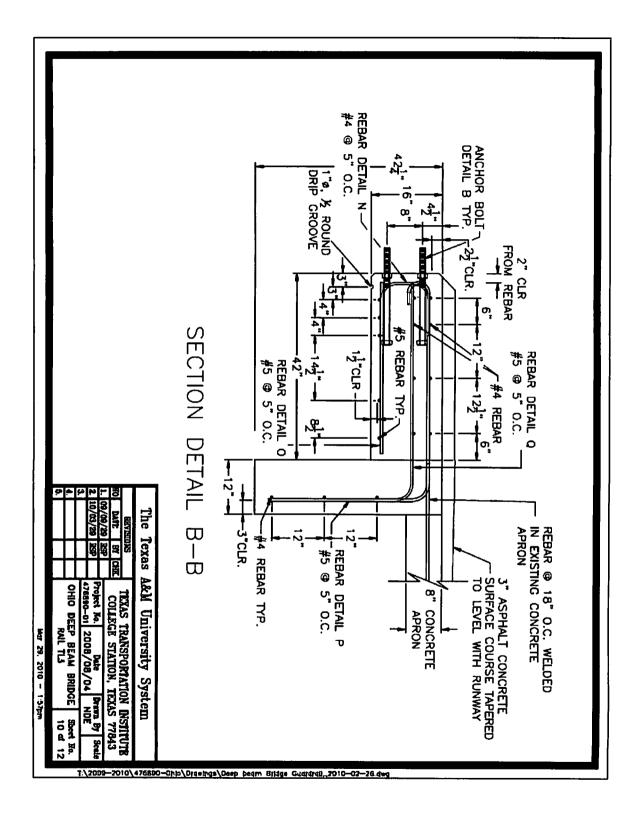


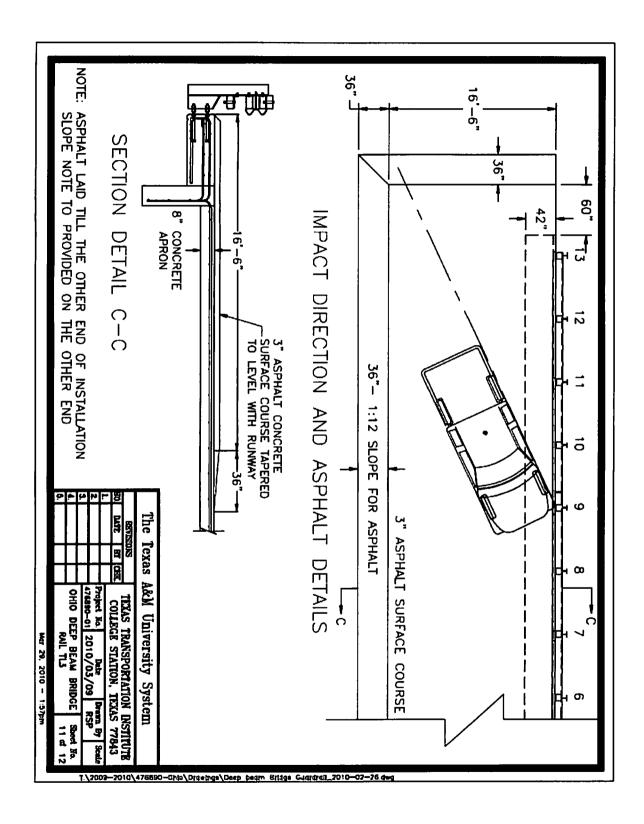


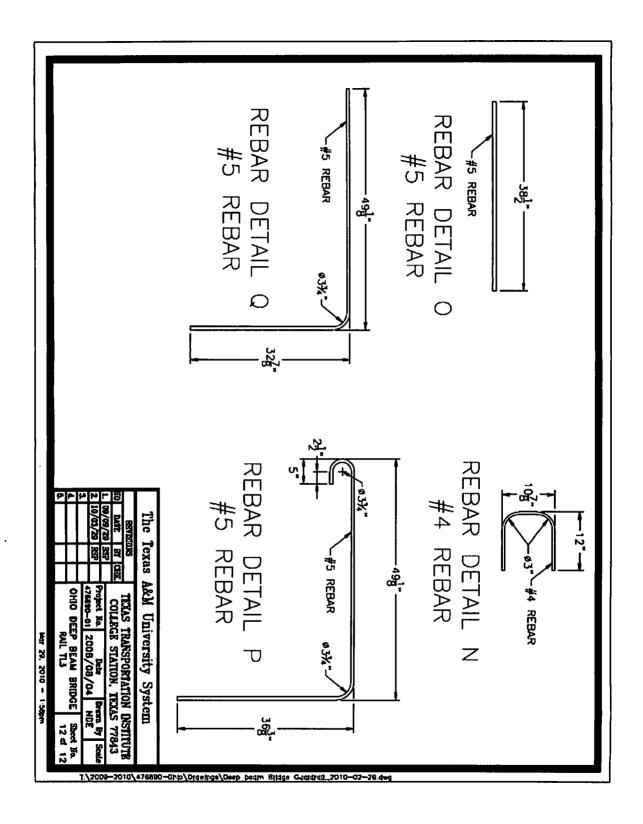




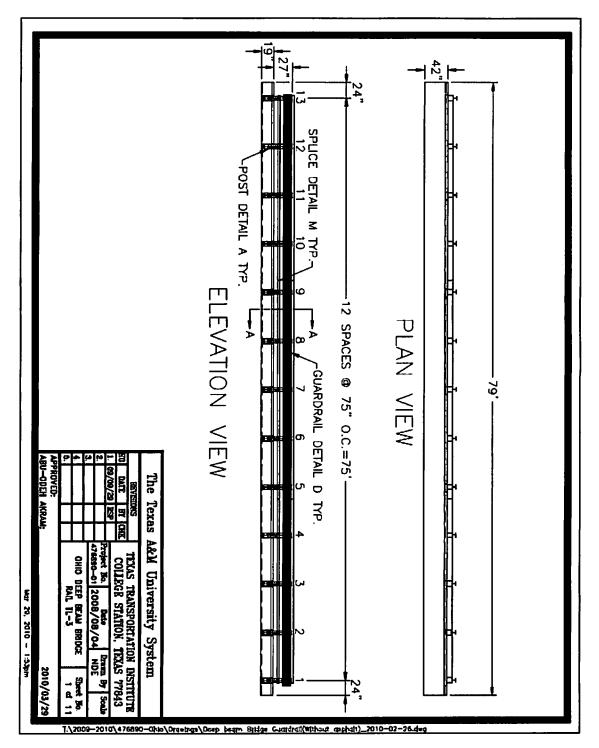












Drawing of ODOT Modified Bridge Rail without Pavement Overlay

